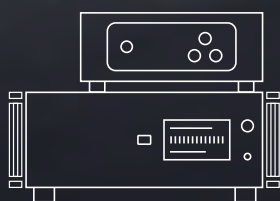
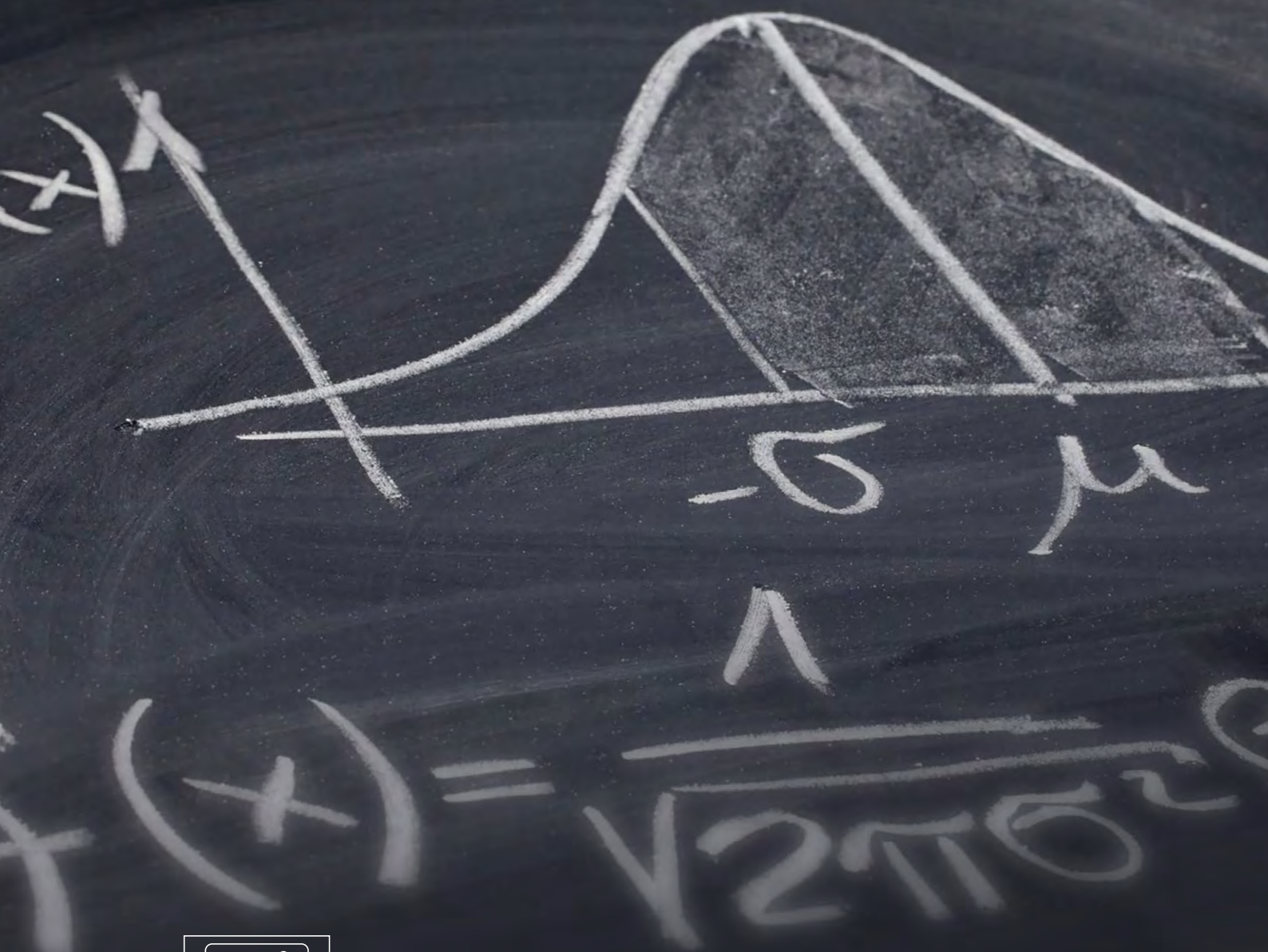




HighFinesse

The Standard of Accuracy



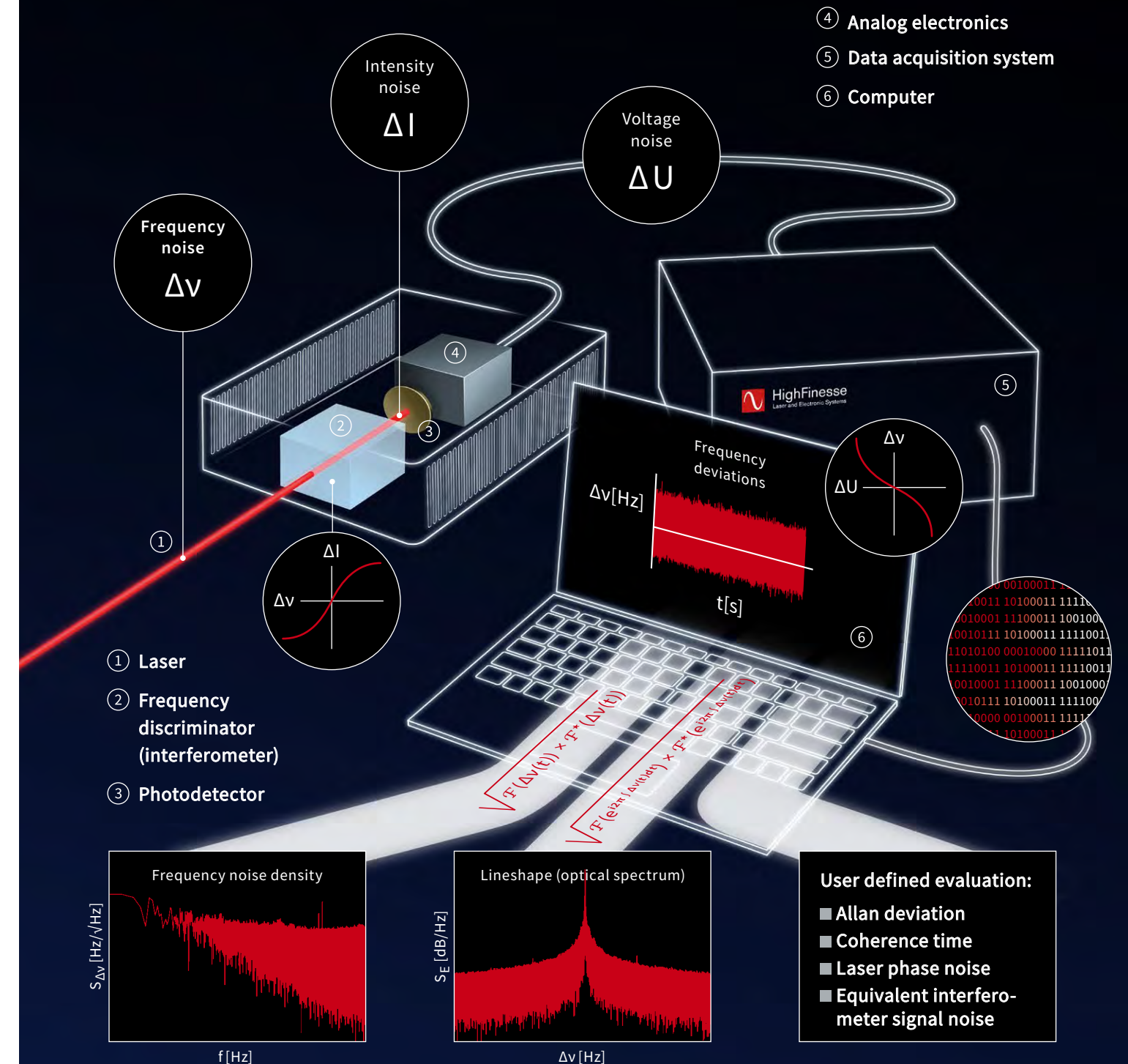
Linewidth Analyzer

High resolution lineshape spectra
and ultra sensitive noise analyzers
for narrowband lasers

The HighFinesse Linewidth Analyzers are the ultimate high-end instruments for measuring, analyzing and controlling frequency of lasers. The superb sensitivity of these instruments is achieved by combining an interferometric working principle with high-end optical and electronic components.

The main features are:

- Frequency noise density, laser phase noise density, optical lineshape analysis with evaluation of intrinsic (Lorentzian) and effective (optical) linewidth
- Intrinsic (Lorentzian) linewidth measurements down to 350 Hz
- Effective (optical) linewidth measurement range down to 1 kHz
- Frequency noise density floor down to 5 Hz/ $\sqrt{\text{Hz}}$ with a dynamic range of 60 dB between 10 Hz and 10 MHz
- Laser phase noise density floor down to 3.2 $\mu\text{rad}/\sqrt{\text{Hz}}$
- Robust against acoustic noise
- Error signal generator for further linewidth, frequency noise reduction
- Powerful tool for a detailed analysis of noise sources like servo bumps, frequency drifts, power supply noise and acoustics
- Extremely fast analysis: up to real time measurements and evaluation



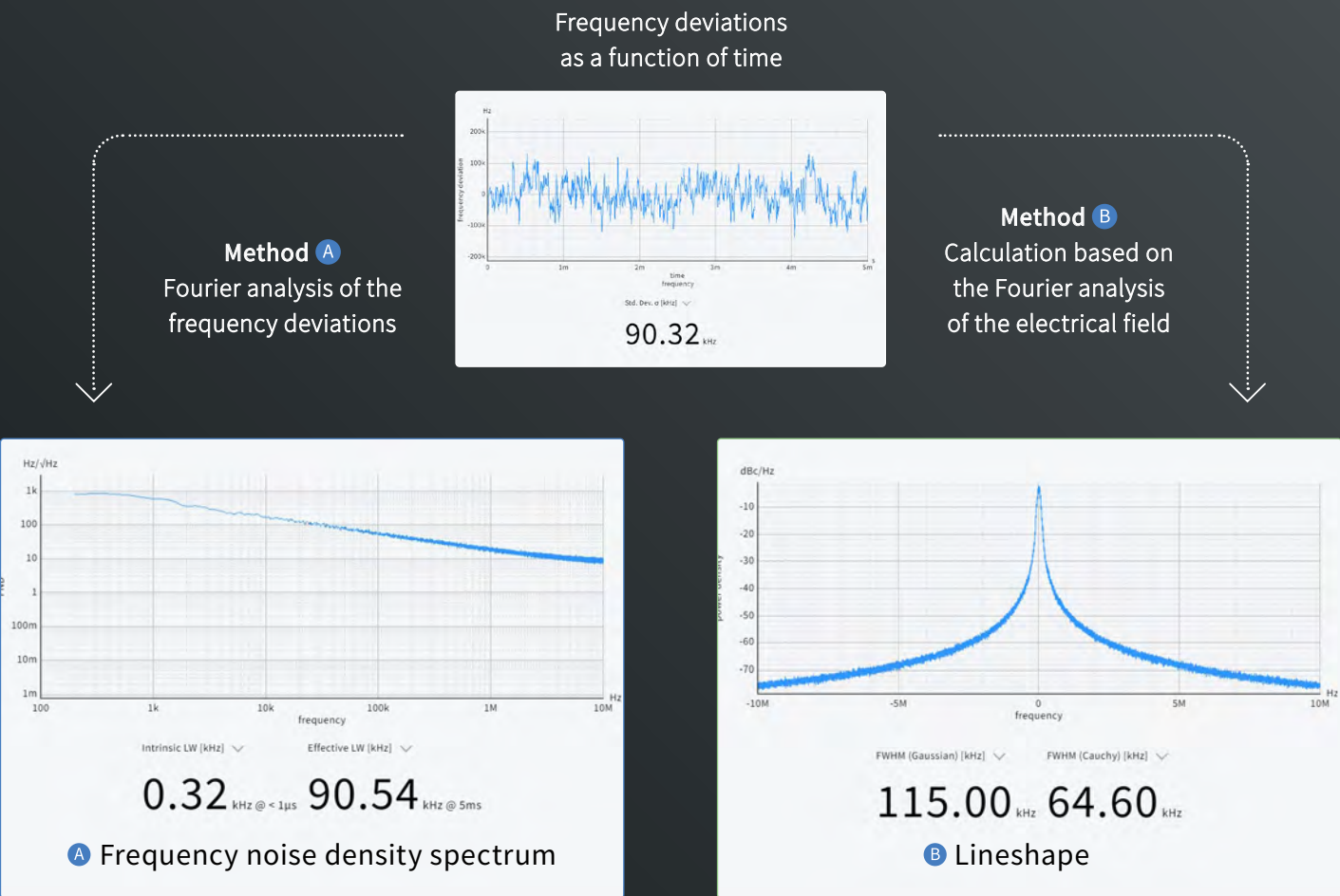
The laser light ① is coupled to the input fiber and lead through an interferometer ② acting as a frequency discriminator. The transmitted intensity, which is directly proportional to the variations of the input frequency, is converted by a photodetector ③ and our analog electronics ④ into a voltage signal.

This voltage is finally digitized by the Digitizer ⑤ to provide the data for evaluation on a computer ⑥. The software suite recovers the original frequency

noise using the precisely known interferometer function. Based on that the software provides the user with the exact frequency noise density, laser phase noise density, and lineshape. From this, the exact frequency noise density, laser phase noise density and line shape are calculated.

The user can also export the timeseries data in order to perform custom evaluation methods such as Allan deviation or coherence time analysis.

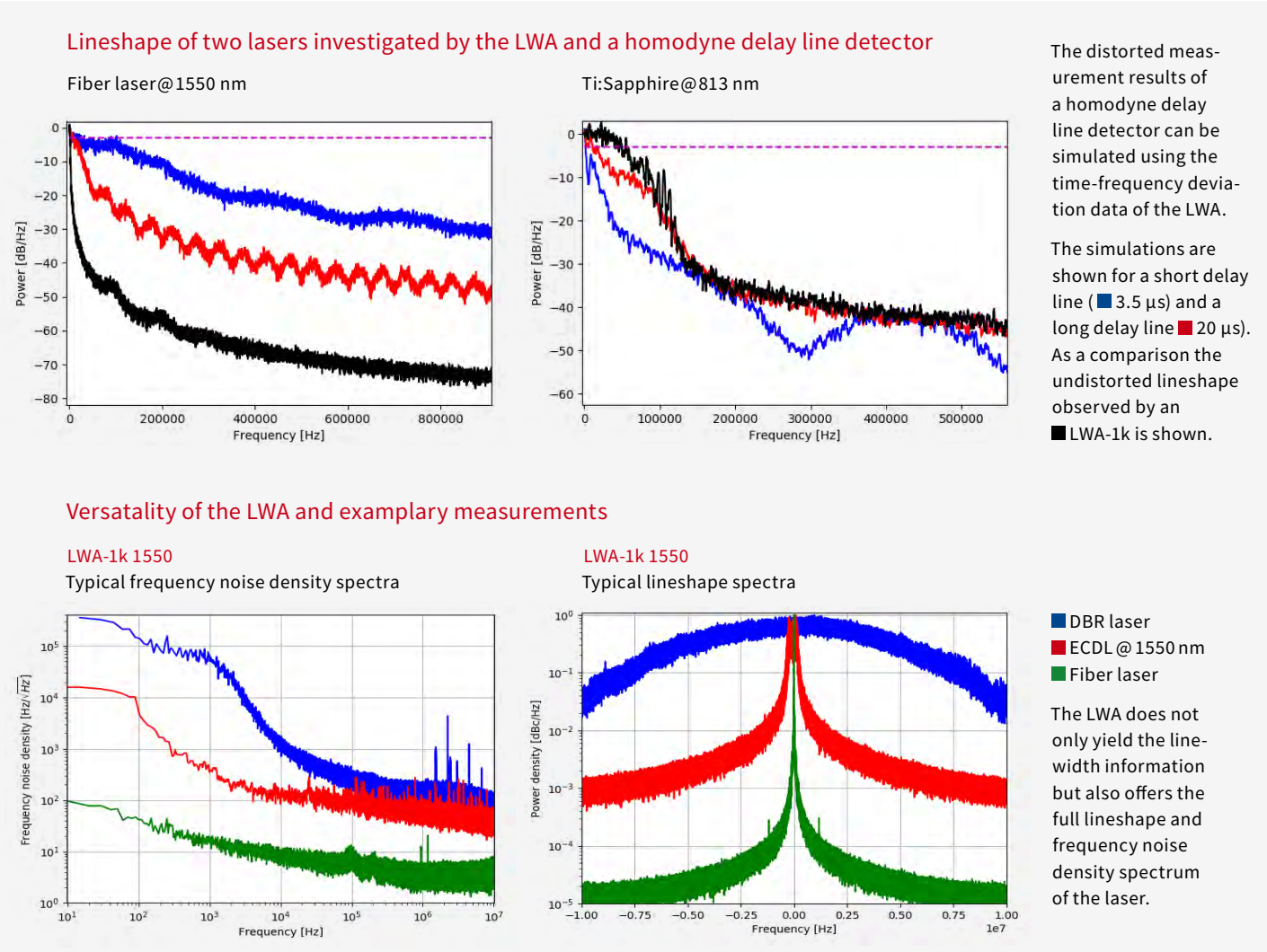
Let the Software Suite do the math for you. The LWA Software Suite is delivered with all LWA products.



- Real-Time Analysis of laser frequency noise
- Automatic calculation of:
 - frequency noise density.
 - laser phase noise density.
 - intrinsic and effective laser linewidth based on the β -separation approach [DiDomenico Appl. Opt. 49 (2010)].
 - optical lineshape for various observation times.
 - linewidth parameters by fitting Voigt, Lorentzian or Gaussian models to the observed lineshape.
- Simple data export to compute: Allan deviation, coherence time, equivalent interferometer signal noise, etc.
- Including programming examples for evaluation of:
 - linewidth parameters by fitting Voigt, Lorentzian or Gaussian models to exported data.
 - Conversion tools.

Comparison: Discriminator- vs. Delay-line-technique

Beside the frequency discrimination approach, homo- and heterodyne delay-line techniques are commonly used for linewidth determination. However, using optical delay lines can lead to complex spectra with non-trivial evaluation needs due to the technique inherent loss of information.



Advantages of the HighFinesse LWA

Principle

Limits

Basic data

Frequency noise density

Lineshape

HighFinesse LWA

Direct frequency noise to intensity conversion

Steepness of discriminator-function

Frequency deviations in time

By a Fourier analysis of the frequency deviations

By a Fourier analysis of the calculated electric fields

Linewidth evaluation

Effective (optical) and intrinsic (Lorentzian) linewidths directly accessible via frequency noise spectrum or lineshape spectrum

Laser phase noise spectrum

By performing a Fourier analysis of the integrated frequency fluctuations

Interferometer signal noise spectrum

By performing a Fourier analysis of the calculated interferometer phase signal¹⁾

Delay-line approach

Optical delayed superposition by different path lengths

Length of delay path

Spectrum of beat note (convolution of original spectrum)

Not possible without additional methods

Lorentzian part (intrinsic linewidth) of the lineshape

Only the Lorentzian part of the linewidth is accessible, because the frequency noise is high-passed by the delay line

Not possible without additional methods

Not possible without additional methods

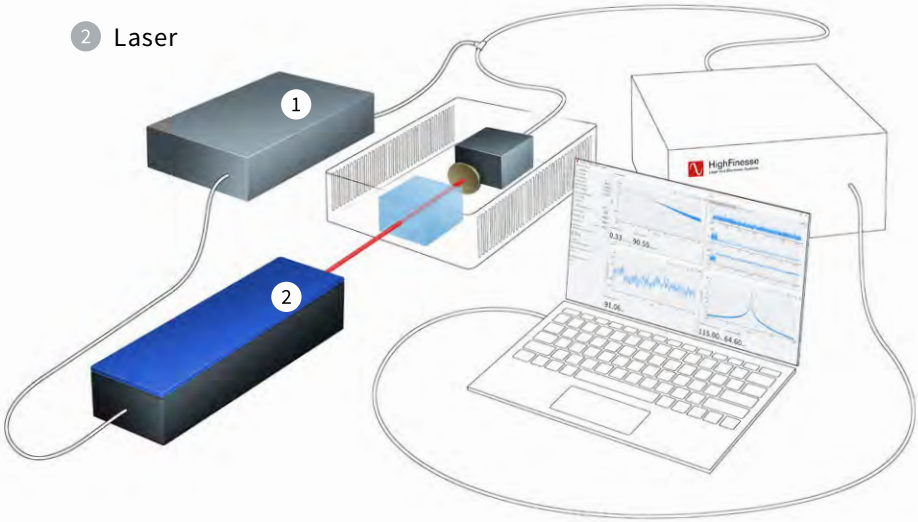
1) Assuming the interferometer working purely as a frequency discriminator and the interferometer phase signal being proportional to the frequency deviation signal.

Feedback Controller

Due to the design of the LWAs, the output voltage can be directly used as an error signal for a feedback controller allowing to reduce the frequency noise of the test laser.

Depending on the used feedback controller and the laser system the optical linewidth can be reduced by more than two orders of magnitude offering a vast amount of new opportunities.

- 1 Feedback controller
- 2 Laser



Active laser noise reduction

- Connect the Analyzer output signal **A** as input signal to a fast feedback controller.
- Connect the feedback controller to the laser’s fast DC modulation input (e.g. laser diode current). **B**
- Adjust the feedback to minimize the output signal of the Analyzer (e.g. PID parameters, gain)

Typical application

- Laser module quality control
- Laser design optimization
- Metrology and quantum technology
- Linewidth control for spectroscopy
- Modulation surveillance

Product Overview

Technical Data

Wavelength range
Input power range (@typical wavelength)
Required input power stability
Laser type
Input fiber type
Maximum frequency stroke (@ f > 10Hz)

Frequency Noise Specification

Noise floor $N_{\Delta\nu}$ @ typ. input power and wavelength ⁶⁾
Laser phase noise floor @typ. input power and wavelength ^{2) 7)}
Equivalent interferometer signal noise @typ. input power and wavelength ^{2) 4)}
Frequency noise bandwidth ⁴⁾
Minimum measurable intrinsic linewidth (lorentzian linewidth @ 1 μ s)
Effective linewidth range (optical linewidth @ 100 ms) [β -separation method]
Relative intensity noise limit (lorentzian linewidth)
Dynamic range

Lineshape Specifications

Effective linewidth range (optical linewidth)
Dynamic range


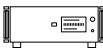


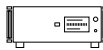
Miscellaneous

Interface
Analog Output
Cutoff (highpass filter)
Dimensions
Weight

Digitizer Module

Sample rate
Resolution
Acquisition time (time series)
Evaluation time ⁵⁾
Communication
Dimensions
Weight

1) Frequency noise and lineshape specifications are derived from measurements at 780 nm.
2) Not included in the software, can be calculated by the user from exported data.
3) According to a -3 dB criterion.

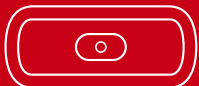
																														
Unit	LWA-1k 780 ¹⁾						LWA-10k VIS ¹⁾						LWA-1k 1550						LWA-10k NIR						LWA-100k NIR					
	min	typ	max				min	typ	max			min	typ	max			min	typ	max			min	typ	max						
nm	760	780	1064				450	780	1064			1530	1550	1625			1064	1550	1625			1064	1550	1625						
mW	1	10	15				0.5	5	8			0.5	5	8			0.5	5	8			0.5	5	8						
%																			± 5											
																			Laser type CW, single mode											
	PM-FC/APC						PM, FC/APC						PM-FC/APC						PM, FC/APC						PM, FC/APC					
MHz	30						40						30						40						100					
Hz	10	100	1k	10k	100k	>1M	10	100	1k	10k	100k	>1M	10	100	1k	10k	100k	>1M	10	100	1k	10k	100k	>1M	10	100	1k	10k	100k	>1M
Hz/√Hz	200	75	30	30	25	15	500	150	60	60	50	30	80	40	15	10	8	5	200	100	30	20	15	10	1k	200	60	50	40	25
rad/√Hz	20	750m	30m	3m	250μ	15μ	5	1.5	60m	6m	500μ	30μ	8	400m	15m	1m	80μ	5μ	20	1	30m	2m	150μ	10μ	100	2	60m	5m	400μ	25μ
dBrad/√Hz	26	-2.5	-30	-50	-72	-96	24	3.5	-24	-44	-66	-90	18	-8	-36	-60	-82	-106	26	0	-30	-54	-76	-100	40	6	-24	-46	-68	-92
rad/√Hz/m	6.2μ	2.3μ	920n	920n	770n	460n	16μ	4.6μ	1.8μ	1.8μ	1.6μ	920n	2.5μ	1.3μ	460n	310n	250n	160n	6.2μ	3.1μ	920n	620n	460n	310n	31μ	7μ	2μ	2μ	2μ	765n
dBrad/√Hz/m	-104	-112	-120	-120	-122	-126	-96	-106	-114	-114	-116	-120	-112	-118	-126	-130	-132	-136	-104	-110	-120	-124	-126	-130	-90	-104	-115	-116	-118	-122
Hz																			10 – 10 M											
Hz	<3 k						<12 k						<350						<2 k						<10 k					
Hz	<10 k – 20 M						<20 k – 30 M						<1 k – 20 M						<5 k – 30 M						<15 k – 100 M					
dB/Hz	–						–						On request only						–						–					
dB													60																	
Hz	<10 k – 10 M						<20 k – 10 M						<1 k – 10 M						<5 k – 10 M						<15 k – 10 M					
dB													60																	
	USB 2.0 Type B						Ethernet						USB 2.0 Type B						Ethernet						Ethernet					
																			BNC ± 7.5 (50Ω) ± 15 (high impedance) V, single ended											
Hz	10, 1k, 10k, 100k						10						10, 1k, 10k, 100k						10						10					
mm	220 × 334 × 96						440 × 340 × 155						220 × 334 × 96						440 × 340 × 155						440 × 340 × 155					
kg	8.0						12						8.0						12						12					
Sa/s																			62.5 M (max.)											
bits																			16											
s																			1 m – 100 m											
s																			10 m – 1 (typ.)											
																			USB 3.0 Type B											
mm																			210 × 200 × 74											
kg																			2.0											

4) This is the calculated noise of the interferometer phase of a two path interferometer with length imbalance L (in meters). The calculation is performed for a given frequency noise density floor by $2\pi nL/c \times N_{\Delta\nu}$, with n being the refractive index of the reference fiber interferometer material and c being the speed of light in vacuum. Values in the table are given for an refractive index of n=1.46 and a reference length of 1 meter.
5) Windows 10 or newer, Intel i5 8600/AMD Ryzen 5 2600 or better, 16GB RAM or more.
6) $N_{\Delta\nu}$ is the noise floor of the instrument in terms of the square root of the power spectral density of the frequency noise.
7) The phase noise floor corresponds to the noise floor of the square root of the power spectral density of the phase. It is calculated from $N_{\Delta\nu}$ by the formula $1/f \times N_{\Delta\nu}$. Additionally, phase noise is often specified in terms of $\mathcal{L}(f)$ which can be calculated with the formula $\mathcal{L}(f) = 1/f^2 \times N_{\Delta\nu}^2/2$.
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Wavelength Meter

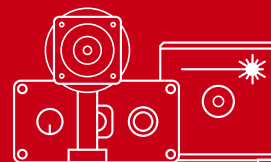
HighFinesse/Ångstrom offers sensitive and compact wavelength meters with a large spectral range for high speed measurement of lasers. The optical unit consists of temperature-controlled Fizeau-based interferometers that are read out by photodiode arrays. The high absolute accuracy is achieved by use of solid state, non-moving optics. The optical unit and associated electronics are housed in a compact, thermal casing. The connection to a computer or notebook is realized via a highspeed USB 2.0 port, which allows a high data read-out rate. The analyzing software displays all the interferometer information.



Spectrometer

The grating based HighFinesse/Ångstrom Laser Spectrum Analyzers offer the capability for a very accurate simultaneous measurement of both the center wavelength and the linewidth of a laser source with a compact and versatile instrument.

The product series covers the ranges from 192 nm to 2250 nm. The grating based technology allows the analysis of laser sources over a large linewidth range. Utilizing the principle of non-moving parts just like the well-known HighFinesse WS-series wavemeters, the LSA offers the time-tested robustness and ability to measure both pulsed and cw lasers.



Calibration Sources

HighFinesse offers a variety of frequency stabilized, narrow linewidth laser sources for the calibration of all wavelength meters and applications down to ± 0.5 MHz absolute accuracy. These are user friendly, plug and play devices that can be connected to the wavelength meter. Different technologies, accuracies and wavelengths are available to suit your application.

HighFinesse stabilized frequency references yield extremely accurate frequency stabilizations, ideal for calibration of our wavelength meters in the visible and infrared wavelength regimes.



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